

APPLICATION STUDY OF POST-TREATED HIGH-STRENGTH STEEL JOINTS IN INDUSTRIAL CRANE FRAMEWORKS

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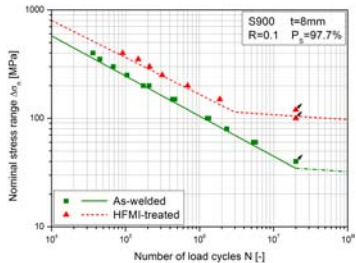
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Introduction

Experimental fatigue tests



- Evaluation of fatigue strength increase by post-treatment methods
- Statistically verified data

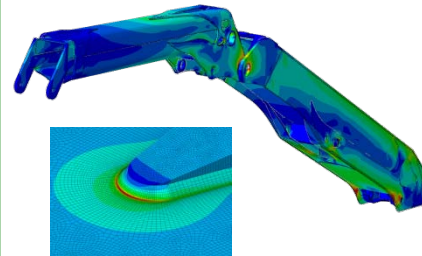
Service load measurements



$$\begin{pmatrix} F_x(t) \\ F_y(t) \\ F_z(t) \end{pmatrix} = \text{Pseudoinv} \begin{bmatrix} \varepsilon_{1,X} & \varepsilon_{1,Y} & \varepsilon_{1,Z} \\ \varepsilon_{2,X} & \varepsilon_{2,Y} & \varepsilon_{2,Z} \\ \varepsilon_{3,X} & \varepsilon_{3,Y} & \varepsilon_{3,Z} \end{bmatrix} \cdot \begin{pmatrix} \varepsilon_{1,\text{measurement}}(t) \\ \varepsilon_{2,\text{measurement}}(t) \\ \varepsilon_{3,\text{measurement}}(t) \end{pmatrix}$$

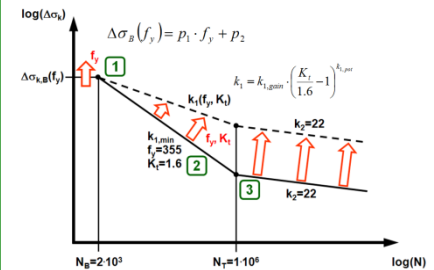
- Built-up of methodology to measure the service loads during operation
- Classification of results

Numerical analysis of structural details



- Numerical analysis of complete structure and critical details by solid, shell and submodels

Local fatigue assessment



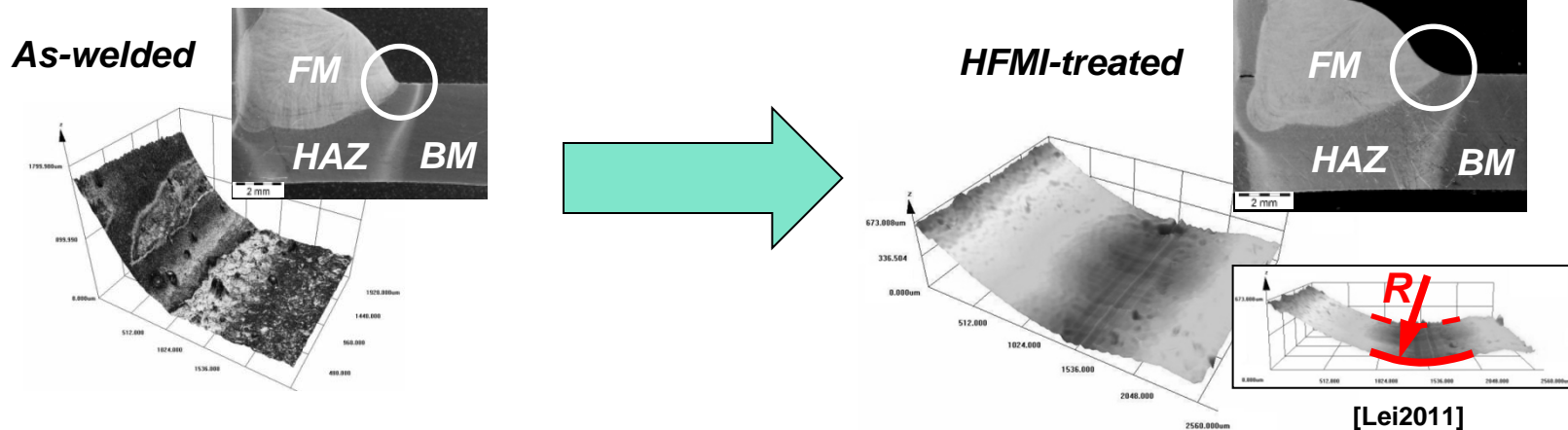
- Local fatigue behaviour of as-welded and post-treated condition
- Lifetime assessment

Light-weight crane frameworks

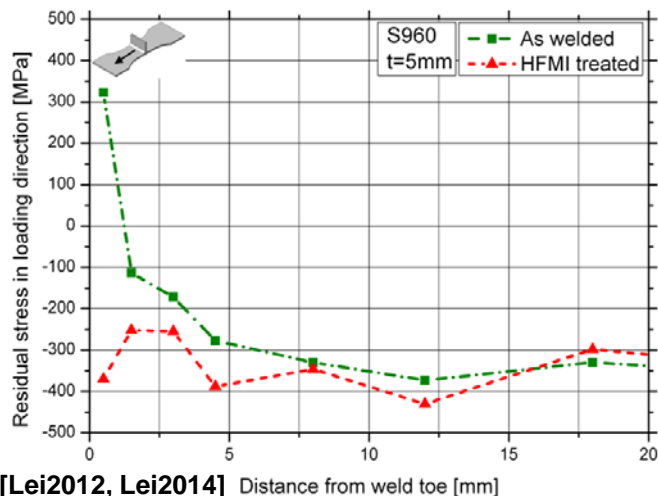


HFMI (High Frequency Mechanical Impact) as post-treatment

Improvement of notch topography



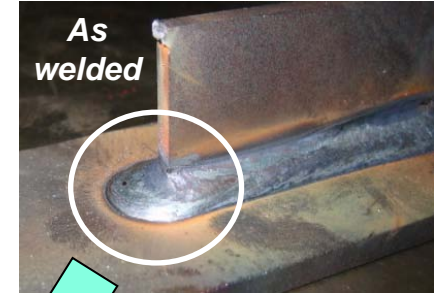
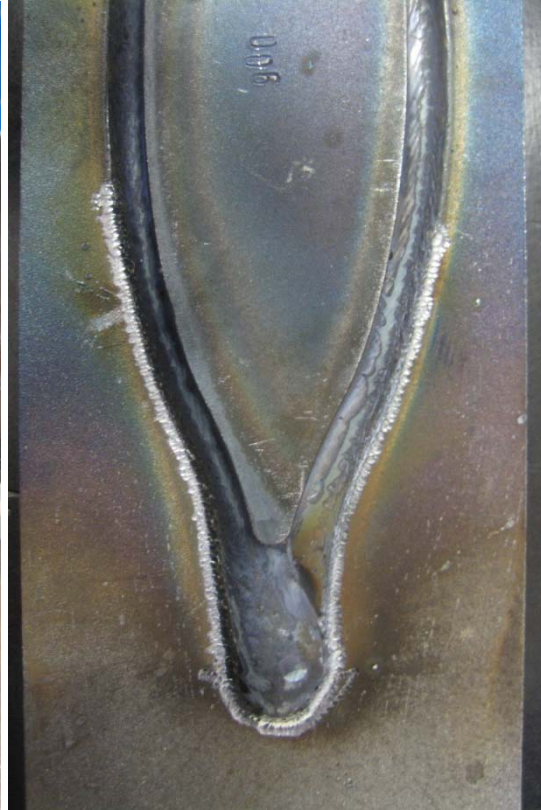
Change of residual stresses



- Surface residual stresses in transversal (load) direction (T-joint, S960)
 - As-welded: High tensile residual stresses at weld toe region (+300MPa)
 - HFMI-treated: Superposition of compressive residual stresses
→ Reduction down to -350MPa

[Lei2012, Lei2014] Distance from weld toe [mm]

End-of-seam specimens – HFMI-treatment



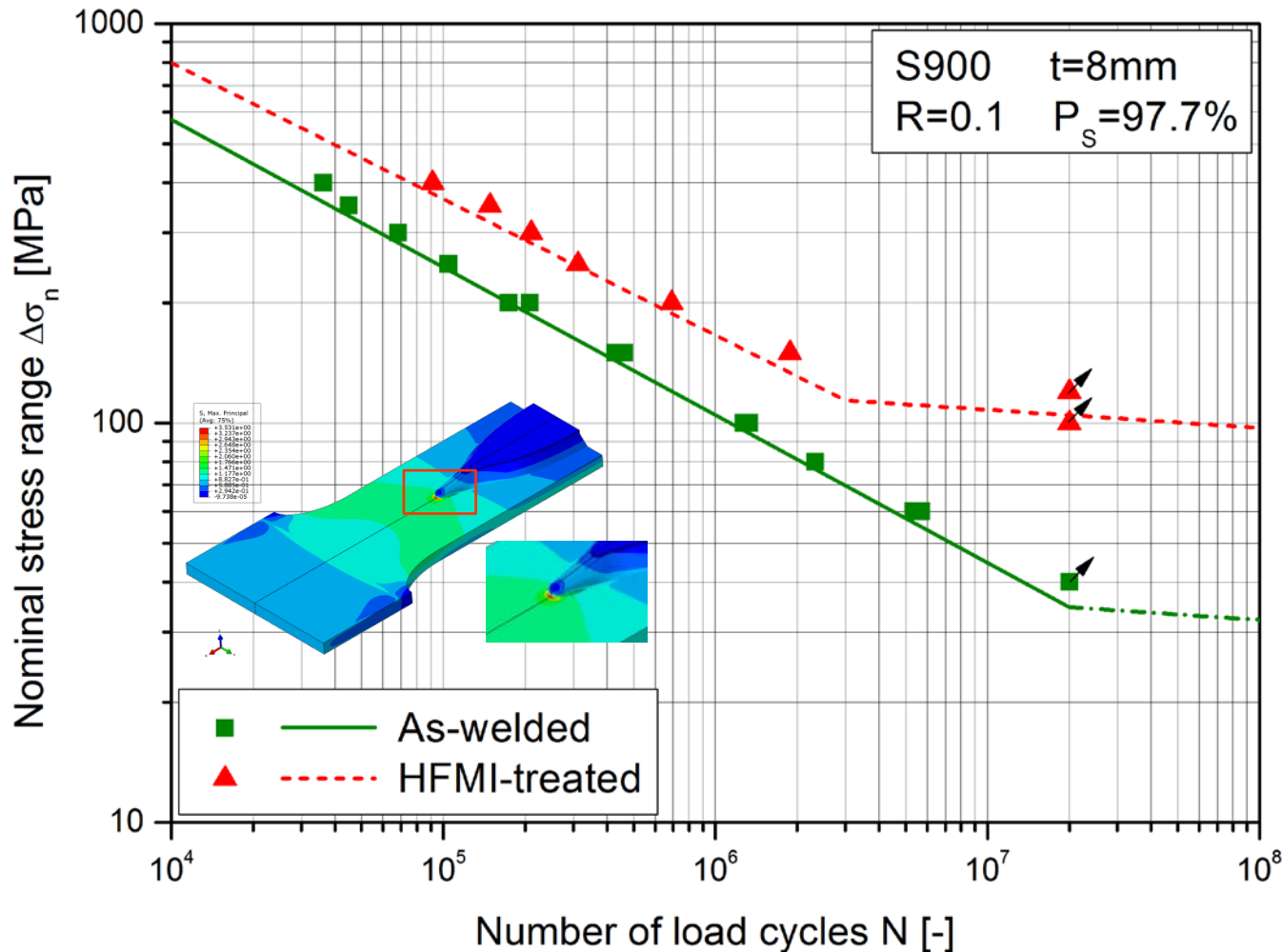
[Lei2011]



[Pit2014]

- HFMI-treatment at the weld toe as post-treatment method (PIT-System)
 - HFMI-Parameters: $p=6\text{bar}$ ($\sim 90\text{psi}$), $v=20\text{-}30\text{cm/min}$, $f=90\text{Hz}$
 - Radius of the hardened pin: $R=2\text{mm}$

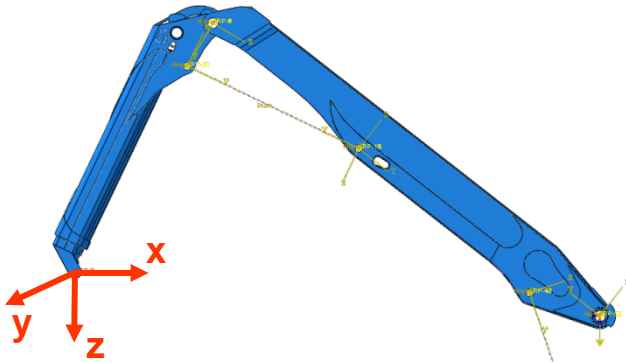
End-of-seam specimens – Nominal S/N-curves



- Major increase of fatigue strength by HFMI-treatment at the weld toe due to high notch effect at weld toe region (small, highly stressed volume)

Service load measurements

- Evaluation of service loads at crane end based on pseudo-inverse approach



$$\begin{aligned} F_X &= \begin{pmatrix} 1 \\ 0 \\ 0 \end{pmatrix} \rightarrow \varepsilon_X = \begin{pmatrix} \varepsilon_{1,X} \\ \varepsilon_{2,X} \\ \varepsilon_{3,X} \end{pmatrix} \\ F_Y &= \begin{pmatrix} 0 \\ 1 \\ 0 \end{pmatrix} \rightarrow \varepsilon_Y = \begin{pmatrix} \varepsilon_{1,Y} \\ \varepsilon_{2,Y} \\ \varepsilon_{3,Y} \end{pmatrix} \\ F_Z &= \begin{pmatrix} 0 \\ 0 \\ 1 \end{pmatrix} \rightarrow \varepsilon_Z = \begin{pmatrix} \varepsilon_{1,Z} \\ \varepsilon_{2,Z} \\ \varepsilon_{3,Z} \end{pmatrix} \end{aligned}$$



Standard load cases
 F_X , F_Y and F_Z

$$\begin{pmatrix} F_X(t) \\ F_Y(t) \\ F_Z(t) \end{pmatrix} = \text{Pseudoinv} \begin{bmatrix} \varepsilon_{1,X} & \varepsilon_{1,Y} & \varepsilon_{1,Z} \\ \varepsilon_{2,X} & \varepsilon_{2,Y} & \varepsilon_{2,Z} \\ \varepsilon_{3,X} & \varepsilon_{3,Y} & \varepsilon_{3,Z} \end{bmatrix} \cdot \begin{pmatrix} \varepsilon_{1,\text{measurement}}(t) \\ \varepsilon_{2,\text{measurement}}(t) \\ \varepsilon_{3,\text{measurement}}(t) \end{pmatrix}$$

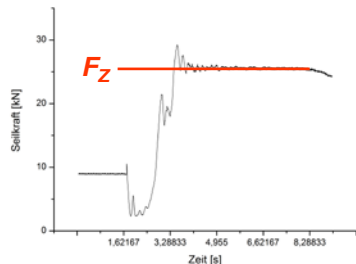


Strain gauge and
cylinder displacement
measurements in service

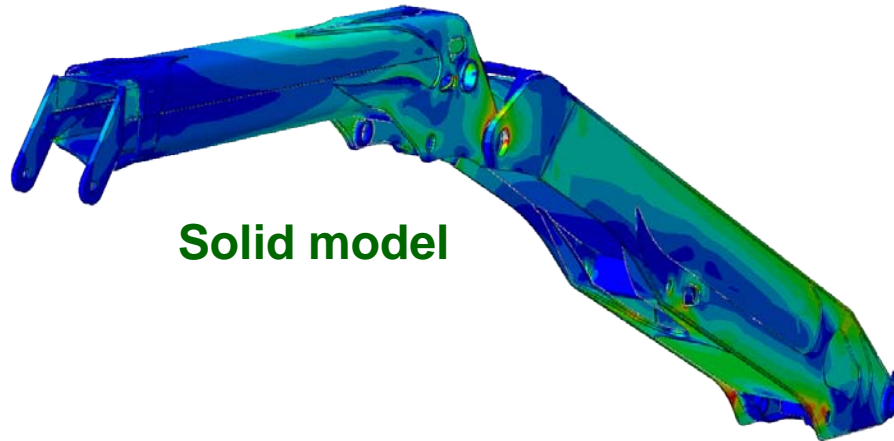


Service loads
 $F_X(t)$, $F_Y(t)$ and $F_Z(t)$

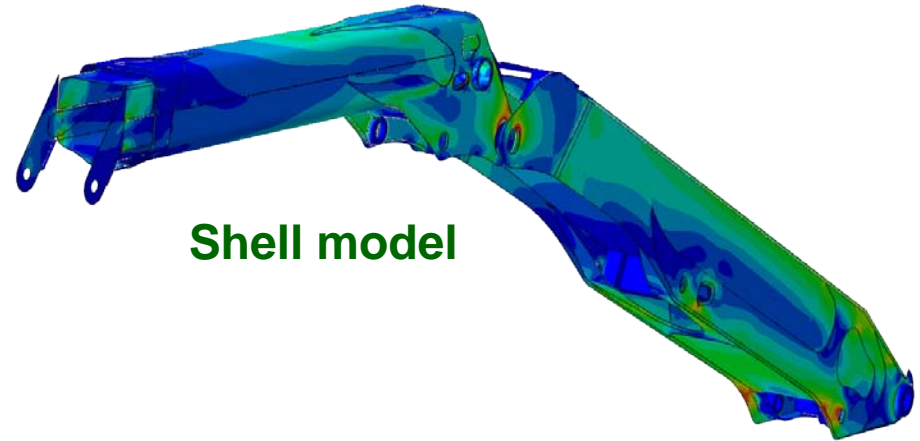
Measurement
of $F_Z \rightarrow \varepsilon_Z$



Numerical analysis – Complete model of framework

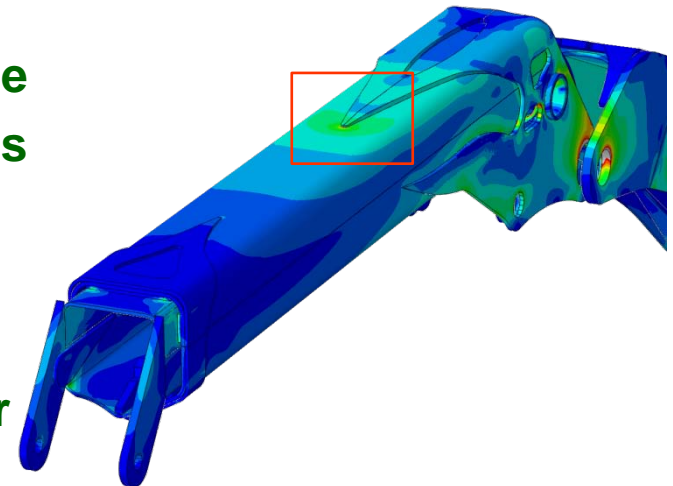


Solid model



Shell model

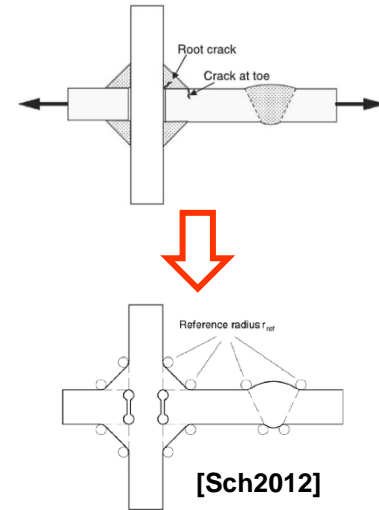
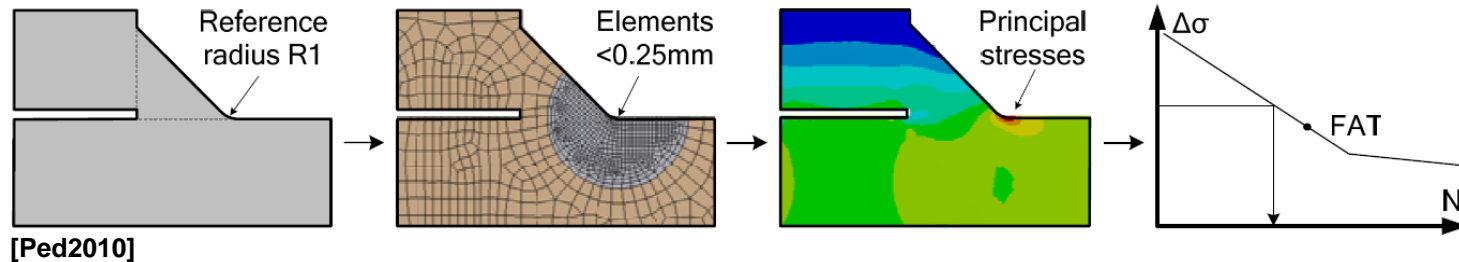
- Built-up of solid and shell model of complete framework
- Good agreement of numerical results between both modeling techniques
- Selection of simulation method depends on
 - Pre-processing effort and computational time
 - Contact modeling between sheets and seams
- Detailed analysis of critical end-of-seam detail by submodeling technique
 - Fine mesh to evaluate local stress behaviour for fatigue assessment properly



Local fatigue assessment

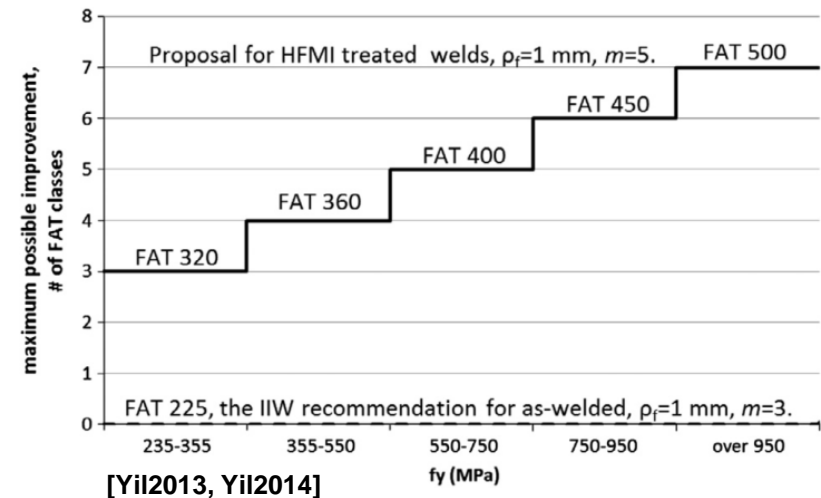
- Effective notch stress concept according to IIW-recommendation [Hob2009]

- Reference radius of $\rho_f=1mm$ based on [Neu1968, Rad1996]
- Slope in finite lifetime region for as-welded condition: $m=3$

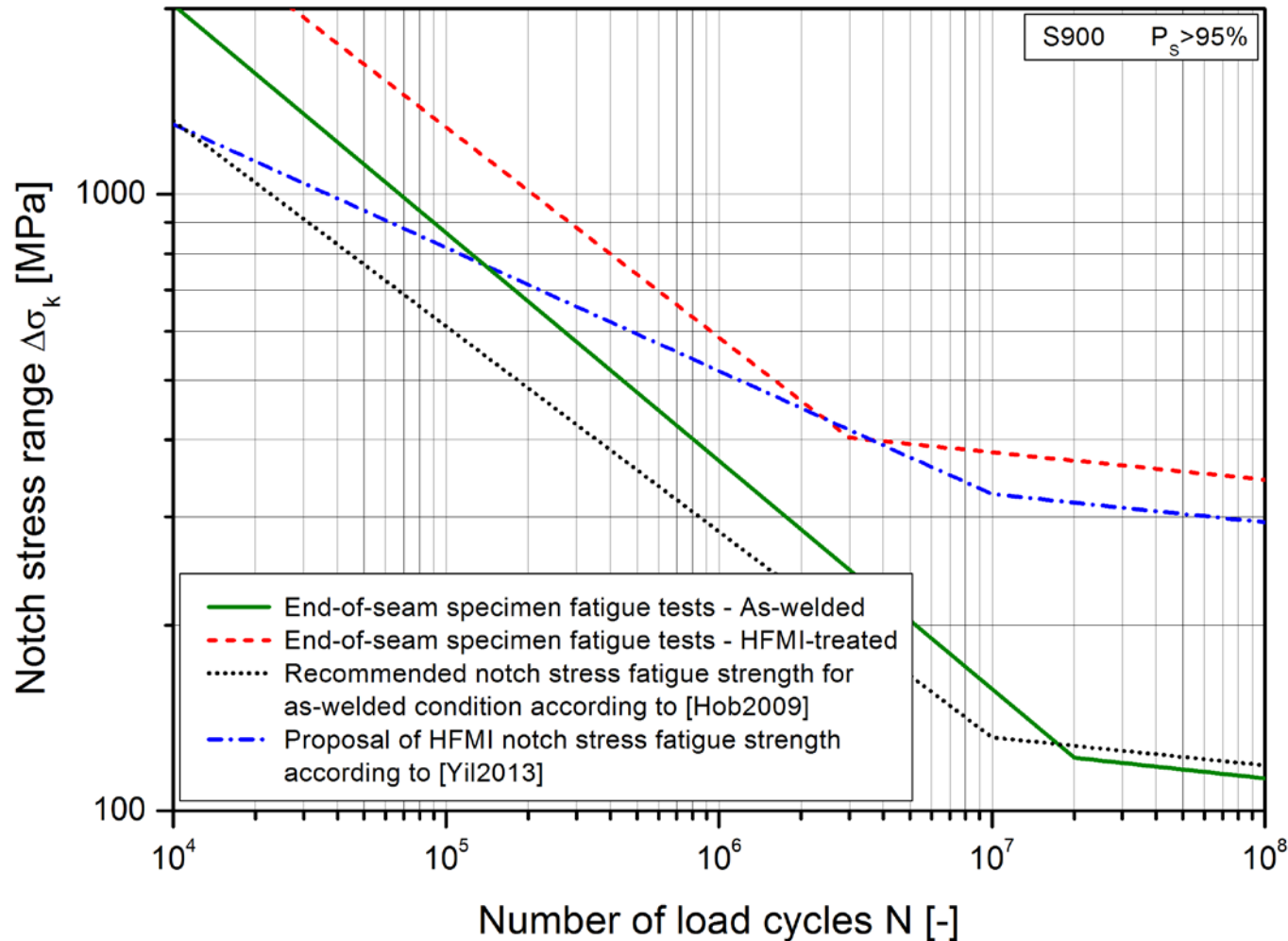


- Proposal of HFMI notch stress fatigue strength according to [Yil2013]

- Reference radius: $\rho_f=1mm$
- Slope in finite lifetime region: $m=5$
- One fatigue class (about 12.5%) increase in fatigue strength for every 200MPa increase in ultimate base material strength f_y



Local fatigue assessment



- Notch stress fatigue assessment shows a good accordance of the fatigue tests and the recommended (as-welded) and proposed (HFMI-treated) values

Summary and Outlook

- Presentation of comprehensive methodology to assess the lifetime of crane frameworks based on experimental fatigue tests, service load measurements, numerical analyses and local fatigue behaviour
- Nominal S/N-curves of investigated HFMI-treated end-of-seam specimens show a significant beneficial increase of the fatigue strength especially in the high-cycle fatigue region up to **250%** compared to the as-welded condition
- Numerical analyses involving solid, shell and submodel technique demonstrate the advantages and drawbacks of each method
- Results of the comparative local fatigue assessment are in good agreement to the proposed HFMI-treatment fatigue guideline

Outlook

- Influence of applied shell elements to study numerical effects
- Determination of stress gradient effect for HFMI-treated joints
- Enhancement of variable amplitude HFMI fatigue test data and implementation in recent guidelines [Mik2013]

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